The separation principle in stochastic control, revisited

Workshop in honor of Eduardo Sontag on the occasion of his 60th birthday

> Tryphon T. Georgiou joint work with Anders Lindquist

linear stochastic system

$$\begin{cases} dx = A(t)x(t)dt + B_1(t)u(t)dt + B_2(t)dw\\ dy = C(t)x(t)dt + D(t)dw \end{cases}$$



w(t) is a vector-valued Wiener process x(0) is a Gaussian random vector independent of w(t), y(0) = 0 A, B_1 , B_2 , C, D are matrix-valued functions

Goal: Design nonanticipatory control

$$\pi : y \mapsto u$$

that minimizes

$$J(u) = E\left\{\int_0^T x(t)'Q(t)x(t)dt + \int_0^T u(t)'R(t)u(t)dt + x(T)'Sx(T)\right\}$$

separation priniciple

under suitable assumptions on the class of admissible control $\pi : y \mapsto u$, the "optimal control" is

$$\begin{split} u(t) &= K(t) \hat{x}(t) \\ \text{where } \hat{x}(t) &= E\{x(t) \mid \mathcal{Y}_t\}, \\ d\hat{x} &= A(t) \hat{x}(t) dt + B_1(t) u(t) dt \\ &\quad + L(t) (dy - C(t) \hat{x}(t) dt) \\ \hat{x}(0) &= 0. \end{split}$$

with K(t) and L(t) computed via a pair of dual Riccati equations

NB:

— attempts to prove separation for u(t) is \mathcal{Y}_t measurable (a.s.)...

- too big a class; we know no proof which is correct (strong solutions)

historical remarks

Wonham, Kushner, Lindquist, Fleming & Rishel

- treatment overburdened with technicalities
- folk accounts not supported by existing proofs
- non-Gaussian nature due to an *a-priori* nonlinear π is often overlooked

• herein, separation principle for:

- the most natural class of controls all linear/nonlinear and even discontinuous such that feedback loop makes "engineering" sense
- engineering view point: signals = sample functions
- general semimartingale driving noise, with jumps
- delay-differential linear systems, etc.



the standard "completion of squares"

$$J(u) = E\left\{x(0)'P(0)x(0) + \int_0^T (u - Kx)'R(u - Kx)dt\right\} + \int_0^T tr(B_2'PB_2)dt$$

where

$$\begin{cases} \dot{P} = -A'P - PA + PB_1R^{-1}B'_1P - Q\\ P(T) = S \end{cases}$$

$$K(t) := -R(t)^{-1}B_1(t)'P(t).$$

using Itô's rule:

$$d(x'Px) = x'\dot{P}xdt + 2x'Pdx + tr(B'_2PB_2)dt = [-x'Qx - u'Ru + (u - Kx)'R(u - Kx) + tr(B'_2PB_2)]dt + 2x'PB_2dv$$

with "complete state-information":

$$u_{\text{optimal}}(t) = K(t)x(t)$$

incomplete state information

u(t) needs to be a function of $\{y(s); 0 \leq s \leq t\}$

Standard recipe:

$$u(t) = K(t)\hat{x}(t)$$

where

 $\hat{x}(t) = E\{x(t) \mid \mathcal{Y}_t\}$

justification \Leftrightarrow *separation theorem*

where is the potential problem?

set

$$\tilde{x}(t) := x(t) - \hat{x}(t)$$

then

$$E\int_0^T (u-Kx)'R(u-Kx)dt = E\int_0^T [(u-K\hat{x})'R(u-K\hat{x})]dt + \operatorname{tr}(K'RK\Sigma)$$

since $E\{[u(t) - K(t)\hat{x}(t)]\tilde{x}(t)'\} = 0$, and where $\Sigma(t) := E\{\tilde{x}(t)\tilde{x}(t)'\}$

why isn't obvious that $u = K\hat{x}$ is optimal?

subtlety: in general, Σ may depend on the control

source of fallacy (?)

due to linearity

$$x(t) = x_0(t) + \int_0^t \Phi(t, s) B_1(s) u(s) ds$$

the control term cancels out:

$$\tilde{x}(t) = \tilde{x}_0(t) := x_0(t) - \hat{x}_0(t),$$

where $\hat{x}_0(t) := E\{x_0(t) \mid \mathcal{Y}_t\}$

how could $E\{\tilde{x}_0(t)\tilde{x}_0(t)'\}$ depend on the control? because the filtration \mathcal{Y}_t , and hence \hat{x}_0 , might depend on u!

- u is in general a nonlinear function of y
- hence, y may not be Gaussian
- despite the fact that x_0 is Gaussian,

 $\hat{x}_0(t) = E\{x_0(t) \mid \mathcal{Y}_t\}$ may not be linear in the data $\{y(\tau); \ \tau \in [0, t]\}$

— $\hat{x}_0(t)$ may not be given by a Kalman filter.

generalization - notation



$$z(t) = z_0(t) + \int_0^t G(t,\tau)u(\tau)d\tau$$
$$y(t) = Hz(t)$$

where

$$g : (t, u) \mapsto \int_0^t G(t, \tau) u(\tau) d\tau$$

E.g., $z(t) = \begin{pmatrix} x(t) \\ y(t) \end{pmatrix}$ and $H = [0, I]$

ways out (?)

SOL: stochastic open loop (Lindquist) limit control so as to be adapted to $\{\mathcal{Y}_t^0\}$



examples

— linear control

— Lipschitz feedback



e.g., control adapted to $\{\mathcal{Y}_t^0\}$ via

example: linear feedback

$$u(t) = u_{\text{deterministic}} + \int_0^t F(t,\tau) dy$$

then the Gaussian character is preserved.

It can be shown that $\mathcal{Y}_t = \mathcal{Y}_t^0$.

Hence,

$$d\tilde{x} = (A - LC)\tilde{x}dt + (B_2 - LD)dw$$

$$\tilde{x}(0) = x(0)$$

 $\Sigma(t) := E\{\tilde{x}(t)\tilde{x}(t)'\}$ is independent of u

$$u(t) = \int_0^t F(t,\tau) dy(\tau) \Rightarrow dy = dy_0 + \int_0^t M(t,s)u(s) ds dt$$
$$\Rightarrow dy = dy_0 + \int_0^t N(t,\tau) dy(\tau) dt$$

where Volterra resolvent Then

$$\begin{split} N(t,\tau) &= \int_{\tau}^{t} M(t,s) F(s,\tau) ds \\ R(t,\tau) &= \int_{\tau}^{t} R(t,s) N(s,\tau) ds + N(t,s) \end{split}$$

$$\begin{split} &\int_0^t N(t,\tau) dy(\tau) = \int_0^t R(t,\tau) dy_0(\tau) \\ \Rightarrow & dy = dy_0 + \int_0^t R(t,\tau) dy_0(\tau) dt \\ \Rightarrow & \sigma\{y(\tau); 0 \leq \tau \leq t\} = \sigma\{y_0(\tau); 0 \leq \tau \leq t\} \end{split}$$

example: Lipschitz continuous control

[Wonham] Assuming that

$$dy(t) = x(t)dt + D(t)dw(t)$$

i.e., ${\cal C}(t)=I$ is invertible! Then among control laws of the form

$$u(t) = \psi(t, \hat{x}(t))$$

the choice $u(t) = K(t)\hat{x}(t)$ is optimal.

[Fleming & Rishel] removed the assumption on C(t); Lipschitz on y; simpler proof.

example: Lipschitz (cont.)

[Kushner]

$$\hat{\xi}_0(t) := E\{x_0(t) \mid \mathcal{Y}_t^0\}$$

given by the Kalman filter

$$d\hat{\xi}_0 = A\hat{\xi}_0(t)dt + L(t)dv_0, \ \hat{\xi}_0(0) = 0$$

$$dv_0 = dy_0 - C\hat{\xi}_0(t)dt, \qquad v_0(0) = 0$$

define

$$\hat{\xi}(t) := \hat{\xi}_0(t) + \int_0^t \Phi(t,s) B_1(s) u(s) ds$$

and assume

 $u(t)=\psi(t,\hat{\xi}(t))$ is Lipschitz

Then $\hat{\xi}$ is the unique strong solution of

$$d\hat{\xi} = \left(A\hat{\xi}(t) + B_1\psi(t,\hat{\xi}(t))\right)dt + L(t)dv_0, \ \hat{\xi}(0) = 0.$$

This choice force u to be adapted to $\{\mathcal{Y}_t^0\} \Rightarrow \{\mathcal{Y}_t^0\} = \{\mathcal{Y}_t\} \Rightarrow \hat{\xi} = \hat{x}$

example: delay in the loop

when u(t) is a function of $y(\tau)$; $0 \le \tau \le t - \varepsilon$, $\mathcal{Y}_t = \mathcal{Y}_t^0$

the possibility of a control-dependent σ -field does not arise in the usual (predictive) discrete-time formulation

- Taking $\epsilon \to 0$ and general nonlinear feedback there is no guarantee that \mathcal{Y}_t is left-continuous
- "Proofs" of separation using such limits are circular, misleading accounts in textbooks.

signals and systems

signals :

sample paths; possibly having bounded discontinuities

in D (càdlàg – Skorokhod space)

systems: measurable nonanticipatory maps

examples:

i) SDE's that have strong solutions ii) nonlinearities, hysteresis ($C \rightarrow D$), etc.





well-posedness of feedback

 \overline{z}

h(z)

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Defn. a feedback loop, that is $z = z_0 + f(z)$ is *well-posed* if it has a unique solution in D for all $z_0 \in D$ and $(1 - f)^{-1}$ is a system.



well-posedness (cont.)

by defn z, z_0 stochastic processes well-posedness implies that

 $\mathcal{Z}_t^0 = \mathcal{Z}_t, \quad t \in [0, T].$

$$(1-f)$$
 and $(1-f)^{-1}$ are systems $\Rightarrow z_0 = z - f(z)$ and $z = (1-f)^{-1} z_0$



NB.

— no more information other than what is contained in \mathcal{Z}_t^0

how about incomplete state-information?



$$z_1 = \begin{pmatrix} w \\ 0 \end{pmatrix}, \quad z_2 = \begin{pmatrix} 0 \\ w \end{pmatrix}$$

generate the same filtrations, i.e., $\mathcal{Z}_t^1 = \mathcal{Z}_t^2$

while for $H = \begin{pmatrix} 1 & 0 \end{pmatrix}$,

$$y_1 = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} w \\ 0 \end{pmatrix}, \quad y_2 = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} 0 \\ w \end{pmatrix}$$

do not, i.e., $\mathcal{Y}_t^1 \neq \mathcal{Y}_t^2$.

linear read-out map u g + z H y π

Assume

$$\begin{aligned} z(t) &= z_0(t) + g \circ \pi(y(t)) \\ y(t) &= H z(t) \end{aligned}$$

is well-posed with H linear,

it follows that

$$\mathcal{Y}_t = \mathcal{Y}_t^0, \quad t \in [0, T].$$

Proof: $(1 - Hg\pi)H = H - Hg\pi H$ $= H(1 - g\pi H)$ $H(1 - g\pi H)^{-1} = (1 - Hg\pi)^{-1}H$ $\Rightarrow y = (1 - Hg\pi)^{-1}y_0$, and $y_0 = (1 - Hg\pi)y$.

essence of the lemma

well-posedness resolves the issue of circular control dependence



the separation principle

thm: assuming

$$\begin{cases} dx = A(t)x(t)dt + B_1(t)u(t)dt + B_2(t)dw \\ dy = C(t)x(t)dt + D(t)dw \end{cases}$$

w(t) is a vector-valued Wiener process x(0) is a Gaussian random vector independent of w(t), y(0) = 0 A, B_1 , B_2 , C, D are matrix-valued functions

there is a unique control law $\pi~:~y\mapsto u$ minimizing

$$J(u) = E\left\{\int_0^T x(t)'Q(t)x(t)dt + \int_0^T u(t)'R(t)u(t)dt + x(T)'Sx(T)\right\}$$

in the class of well-posed control laws, and has the form

$$u(t) = K(t)\hat{x}(t)$$

the separation principle (general)

thm: for the same linear system, assuming w is a *semimartingale* and x(0) an independent random vector the unique optimal control in the class of well-posed controllers is given by

 $u(t) = K(t)\hat{x}(t)$

where \hat{x} is the conditional mean.

remarks: no need for Lipschitz continuity allows jump processes K(t) is still given by a Riccati equation in general, the difficult part is constructing $\hat{x}(t) = E\{x(t)|\mathcal{Y}_t\}$. **Proof:** i) $\mathcal{Y}_t = \mathcal{Y}_t^0$, $t \in [0, T]$.

ii) completion-of-squares using Itô's rule:

$$x(T)'Px(T) - x(0)'Px(0) = f_{\Delta} + \int_0^T \{x'\dot{P}xdt + 2x'Pdx + d\operatorname{tr}([x, x']P)\}$$

 \Rightarrow

iii) $x(t) = \int_0^t \Phi(t,s) (A(s)x(s) + B_1(s)u(s)) ds + v(t)$ i.e., continuous/BV +v(t) where $dv = B_2 dw$

iii_a)
$$[x, x'] = [v, v']$$
 independent of u
iii_b) $f_{\Delta} = \sum_{s \leq T} \left[(x(s)'P(s)(x(s) - x(s_{-})'P(s)x(s_{-}) -2x(s_{-})'P(s)\Delta_s - \Delta'_s P(s)\Delta_s) \right]$
 $= 0$

where $\Delta_s := x(s) - x(s_-)$.

example: step change in white noise



$$v(t) = \begin{cases} 1 & t \ge \tau \\ 0 & t < \tau \end{cases}$$

with τ exponentially distributed

minimize $E\left\{\int_{0}^{T} (x^{2} + u^{2})dt\right\}$ $\begin{cases} dx = u(t)dt + dv, \ x(0) = 0, \\ dy = x(t)dt + dw \end{cases}$ i) Wonham-Shiryaev filter:

$$d\hat{x} = (1-\hat{x})dt + udt + \hat{x}(1-\hat{x})(dy - \hat{x}dt)$$

ii) optimal feedback:

$$u(t) = -p(t)\hat{x}(t)$$

where $\dot{p} = p^2 - 1 \Rightarrow p(t) = \tanh(T - t)$.

iii) cost: since [v, v](t) = v(t),

$$E\left\{\int_0^T p(t)d[v,v](t)\right\} = E\left\{\int_\tau^T p(t)dt\right\}$$
$$= \ln(\cosh T)(1-e^{-T}) - \int_0^T \ln(\cosh t)e^{-t}dt.$$

separation for delay-differential systems

$$\begin{cases} dx = A_1(t)x(t)dt + A_2(t)x(t-h)dt \\ + \int_{t-h}^t A_0(t,s)x(s)dsdt + B_1(t)u(t)dt + B_2(t)dw \\ dy = C_1(t)x(t)dt + C_2(t)x(t-h)dt + D(t)dw \end{cases}$$

more generally

$$\begin{cases} dx = \int_{t-h}^{t} d_s A(t,s) x(s) dt + B_1(t) u(t) dt + B_2(t) dw \\ dy = \int_{t-h}^{t} d_s C(t,s) x(s) dt + D(t) dw \end{cases}$$

determine π to minimize

$$E\left\{\int_0^T x(t)'Q(t)x(t)d\alpha(t) + \int_0^T u(t)'R(t)u(t)dt\right\}$$

System can be written in the form:

$$z(t) = z_0(t) + \int_0^t G(t,\tau)u(\tau)d\tau$$
$$y(t) = H(t)z(t)$$

Deterministic optimal control

Deterministic optimal control problem (with w = 0) is

$$u_{\text{optimal}}(t) = \int_{t-h}^{t} d_{\tau} K(t,\tau) x(\tau)$$

separation thm for delay systems

w a Gaussian martingale over all feedback laws π that are well-posed the unique optimal control law is given by

$$u(t) = \int_{t-h}^{t} d_s K(t,s) \hat{x}(s|t)$$

with

$$\hat{x}(s|t) := E\{x(s) \mid \mathcal{Y}_t\}$$

is given by a linear (distributed) filter [Lindquist]

$$\begin{aligned} d\hat{x}(t|t) &= \int_{t-h}^{t} d_{s}A(t,s)\hat{x}(s|t)dt + B_{1}udt + X(t,t)dv \\ d_{t}\hat{x}(s|t) &= X(s,t)dv, \ s \leq t \\ dv &= dy - \int_{t-h}^{t} d_{s}C(t,s)\hat{x}(s|t)dt, \ v(0) = 0 \end{aligned}$$

Key points

- well-posedness + linearity \Rightarrow control-independent σ -field
- separation principle holds over a wide class of nonlinear control: $u = K\hat{x}$ is optimal
- noise: semi-martingale with possible jumps

Happy birthday Eduardo!!!